Electroplating of Carbon Nanotube Yarns and Tapes with Five Metals

by
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ABSTRACT

Carbon nanotube (CNT) tapes and yarns can reduce the weight of industrial cables for aviation and space by substituting for copper. In order to attach the CNTs to cable connectors, one high-reliability method of attachment is soldering. Soldering to CNTs is extremely difficult; however it is facilitated by electroplating the CNT with solderable metals. In this study, CNT tapes and yarns were electroplated with copper, silver, nickel, tin and gold. Electrodeposition rates of CNT yarns were 5.5, 3.9, 6.7, 19.9, and 0.64 μm/min, on copper, silver, nickel, tin and gold, and on CNT tapes similar numbers scaled down by area. Best surface treatment, current, loading, temperature, concentration, additives, correct anode, and their effect on efficiency, deposition rate and adhesion were determined. Adhesion of copper films improved markedly over 15 μm thickness. Multiple samples of up to five at a time were deposited by scaling up the current by the number of samples. The $C_p$ value was 3.4 for copper, indicating copper plating was repeatable.

Keywords: CNT, carbon nanotube, electroplating, adhesion, SPC, current efficiency, soldering, attachment.

Introduction

Carbon nanotubes (CNTs) are a widely studied allotrope of carbon. Their size-to-length ratio creates unique physical properties, such as tensile strength and conductivity, which outperform common bulk materials. Possible applications of CNTs are energy storage, interconnects for CMOS and sensors.1 Military and commercial aircraft and satellites have miles of cable that are used for transmitting signals and power. Carbon nanotube (CNT) tapes and yarns are lightweight conductive materials that show potential for signal and current carrying capacity. These light-weight materials could enable military and commercial aircraft and satellites to travel further on less fuel. By replacing copper in a cable with CNT materials, the weight of a cable assembly can be reduced 70%.2 While mechanical crimps are an adequate termination strategy, soldering directly onto the CNT materials is not possible due to their hydrophobicity.3,4 By metallizing the CNT via electroplating and/or electroless plating metals, soldering is possible. TE Connectivity™ is researching the replacement of copper in cable assemblies, and has already used CNTs for USB cables.

Theory

Discovery and demonstration

The first mention of a carbon filament from the decomposition of methane is credited to Edison in 1889 in an electric light bulb patent.5 The first TEM image of tubular carbon filaments was published in Russian (Fig. 1).6 Iijima7 is given credit for demonstrating the presence of CNTs in the cathode arc in electric arc trials intended to create fullerenes (C60). A survey article of the history of carbon nanotubes, graphene and fullerenes appeared in Carbon in 2006.6 The authors discuss the almost simultaneous identification of single-walled CNTs (SWCNTs) at IBM by Bethune8 in 1993, and Iijima and Ichihashi,7 published a month earlier.

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Figure 1 - First TEM of a CNT, multi-walled\(^6\) (reprinted with permission).

Structure

Anantram and Leonard\(^9\) studied the structure of CNTs. They found armchair, zigzag and chiral structures. The multiwall carbon nanotube structure consists of multiple single-wall CNTs (SWCNTs) inside each other like a Russian doll, with the interplanar distance being similar to the interplanar distance of graphite. With no dangling bonds, each carbon atom is bonded to three nearest neighbors, all sp\(^2\)-double bonded. Although the conduction mechanism is complex in large-format CNTs (tapes and yarns), SWCNT and MWCNT (multiwall CNT) exhibit exclusively metallic conduction in armchair, and either metallic or semiconducting conduction in zigzag and chiral configurations (Fig. 2).

Figure 2 - (a) Zigzag carbon nanotube, (b) armchair and (c) chiral structures\(^9\) (reprinted with permission).

Functionalization

Carbon nanotubes can be modified to contain R-COOH groups when treated in nitric and sulfuric acid,\(^9\) according to theory. Moreover, 1-3\% of the carbon atoms are at defective five-carbon rings, known as Stone-Wales defects, as shown in Fig. 3, where chemical attachment can occur.\(^9\) Thermal oxidation can produce the aforementioned R-COOH group, as shown in Fig. 4.\(^10\) Rafieem, et al.\(^11\) modified the surface of graphene to obtain hydrophilic (wetting) graphene by sonicating in water, and hydrophobic by sonicating in acetone. Oxidation and plasma activation can also modify this property,\(^11\) as well as amidization. Basiuk, et al.\(^12\) treated carbon nanotubes with amine vapor at 170°C in reduced pressure to amidize the R-COOH group.
Since the C=C bonds in CNTs are not reactive, the R-COOH molecules are reactive groups which could be used for attaching plating metal ions after reduction. Balasubramanian found that for functional groups, Raman peaks for radial breathing mode intensity increased, indicating hexagonal lattice disturbance; and the D-or disorder peak also increased in intensity. Atomic force microscopy (AFM) confirmed the existence of the functional group. It is by activation of these functional groups that electroplating should occur, by means of preclean and chemical functionalization in the plating solution.

Experimental

Wetting angles were measured with the Rame-Hart drop angle tester. The cleaning procedure was then executed in two steps, one for degreasing and one for cleaning. Tapes/yarns were then subjected to various chemicals commonly found in electroplating and electroless plating. Selection of parameters and their values, as well as chemical mixtures and conditions, were made iteratively based upon results.
Results and discussion

Summary

Continuous, adherent films were demonstrated with commonly available chemicals from plating suppliers. Multiple tapes and/or yarns were plated, simultaneously, electrolytically or electrolessly. In electroplating all tapes/yarns need to be connected to the cathode in parallel. In electroless plating, the rate depends upon total amount of surface area and chemistry. In an industrial process, ideally hundreds of tapes/yarns might be plated at the same time. This is because tapes/yarns only need to be plated on the ends for soldering. CNTs have one ohm/inch resistivity presently, and by embedding metals will eventually lead to much lower resistivity.

Plating results

Electroplated tapes and yarns are shown in Fig. 5. SEM cross sections are shown in Figs. 6 and 7. As expected, metal area had bright appearance under backscattered electrons due to higher electron fluorescence, while carbon nanotube and potting compound appear dark. The black square indicates an analysis spot (plated metal) for SEM. The electrodeposition rates are shown in Fig. 8.

Figure 5 - Carbon nanotube tapes and yarns, electroplated with (L-R): Copper, silver, nickel, tin with high concentration, tin with low concentration, and gold. The plated area is approximately 4 in. (10 cm) long.

Figure 6 - Backscatter SEM and EDX of silver cross-section (Square).
Figure 7 - Backscatter SEM and EDX of nickel cross-section (top); tin (bottom).

Figure 8 - Electrodeposition rates.
Wetting and adhesion

Pre-plating wetting can be tested by contact angle. Hydrophobic surfaces produce a higher contact angle in a liquid, hydrophilic a lower angle. Yarns/tapes were cleaned in a two-step process. This treatment caused the yams/tapes to degrease (increased contact angle) then wet (decreased contact angle). Acetone was used to degrease, 10% sulfuric acid to wet. For basic plating solution (silver), KOH was substituted for sulfuric.

Adhesion was tested on tapes using ASTM D3359, using a crosscut kit. Figure 9 shows that for copper-nickel (nickel plated over copper) and copper, adhesion was excellent. Yarns were penetrated by the metal, shown in SEM in Fig. 10, indicating adhesion was also excellent.

Development of deposition conditions

Deposition conditions were developed iteratively with thickness results. Variables that were evaluated were: type of substrate (yarn or tape), anode type, current, one-or two-step deposition, number of samples (loading), temperature, and concentration of acid. Early in experimentation stirring was eliminated as a variable because stirred electroplated solutions did not adhere, presumably because nucleation was too slow. Multiple step depositions were required for silver, tin and nickel. Silver was found to require a different concentration acid in the first step. These multiple step depositions are referred to as strike and deposit. Plating solutions and conditions are found in Table 1.
Multilayer films

Five film combinations were successfully deposited in layers: Cu-Ni-Sn, Cu-Ni-Au, Cu-Ni-Ag, Cu-Ni, Cu-Sn, and Cu-Ag (Fig. 11). At the onset of copper deposition, Cu-Ag had to be dipped into the silver plating solution with the current on to avoid the copper dissolving in the basic silver plating solution.

Multilayer films were intended to solder better than single layer films, e.g., CuNiSn, a common solder film. Nickel is a diffusion barrier between copper and tin. Used in solder bump for silicon-metal bond pads, copper sticks to the surface of the soldered item, and tin interacts metallurgically with solder. Cross-section SEMs (Fig. 12) of multilayer films showed there was no layer structure. This is explained by the porous open nature of carbon nanotube macrostructure, in which a film might deposit anywhere in the volume not necessarily on top of the previous film. Therefore single layer structures would be preferred.

Table 1 - Plating conditions.

<table>
<thead>
<tr>
<th>Film</th>
<th>Acid/ Base</th>
<th>Chemistry</th>
<th>Temperature</th>
<th>Strike?</th>
<th>CURRENT (mA)</th>
<th>additives</th>
<th>anode</th>
</tr>
</thead>
<tbody>
<tr>
<td>copper</td>
<td>Acid</td>
<td>Copper sulfate</td>
<td>room</td>
<td>NO</td>
<td>200</td>
<td>none</td>
<td>Phosphorized 99.999% copper</td>
</tr>
<tr>
<td>silver</td>
<td>Base</td>
<td>Silver Succinate</td>
<td>50° C</td>
<td>YES</td>
<td>30</td>
<td>Brightener, leveler</td>
<td>99.99% Silver</td>
</tr>
<tr>
<td>nickel</td>
<td>Acid</td>
<td>Nickel Sulfamate</td>
<td>50° C</td>
<td>YES</td>
<td>300</td>
<td>wetting and hardening agents</td>
<td>nickel or platinum</td>
</tr>
<tr>
<td>tin</td>
<td>Acid</td>
<td>Tin Sulfate</td>
<td>40° C</td>
<td>YES</td>
<td>300</td>
<td>none</td>
<td>tin</td>
</tr>
<tr>
<td>gold</td>
<td>Acid</td>
<td>Gold Sulfite</td>
<td>57° C</td>
<td>NO</td>
<td>30</td>
<td>none</td>
<td>stainless steel, platinum, gold</td>
</tr>
</tbody>
</table>

Figure 11 - Thicknesses of multilayer films.
Figure 12 - Copper, nickel and tin in same location, therefore no layers.

Repeatability

The calculation of weight gain/minute allows yarn and tape data to be combined. The average, standard deviation and standard deviation/average for electroplated films, are shown in Table 2.

Copper had a $C_p$ of 3.4 which is extremely high. $C_p$ is a measure of process repeatability\(^\text{13}\) as defined in Equation 1:

$$C_p = \frac{USL-LSL}{6\sigma}$$

(1)

The specification range defines what is expected in range, that is, upper limit-lower limit. The purpose of these films is to solder to connectors, therefore a wide range would be expected. LSL is the lower specification limit; USL is upper limit. The copper SPC control chart is shown in Fig. 13.

Table 2 - Deposition rate (average value) of films in mg/minute; standard deviation and standard deviation/average; population (number of samples).

<table>
<thead>
<tr>
<th>film</th>
<th>dep rate, mg/minute</th>
<th>Std. dev.</th>
<th>Std. dev/average</th>
<th>population</th>
</tr>
</thead>
<tbody>
<tr>
<td>copper</td>
<td>4.08</td>
<td>0.39</td>
<td>0.09</td>
<td>33</td>
</tr>
<tr>
<td>silver</td>
<td>3.9</td>
<td>0.86</td>
<td>0.22</td>
<td>29</td>
</tr>
<tr>
<td>nickel</td>
<td>5.04</td>
<td>1.61</td>
<td>0.32</td>
<td>37</td>
</tr>
<tr>
<td>tin</td>
<td>10.77</td>
<td>2.88</td>
<td>0.27</td>
<td>15</td>
</tr>
<tr>
<td>gold</td>
<td>1.68</td>
<td>0.84</td>
<td>0.84</td>
<td>16</td>
</tr>
</tbody>
</table>
Development of thinner films

As outlined earlier, adhesion was excellent. Figure 14 shows a top-down backscatter SEM of a copper sample, with 5 \( \mu \)m of copper film. As shown in Table 3, adhesion suffers for films of less than 10 \( \mu \)m. To save on materials, time and cost, all industrial processes seek to optimize parameters, in this case lower thickness. To this end, adhesion of copper was tested at different thicknesses. A top down SEM (Fig. 14) shows that copper coverage below a 5 \( \mu \)m thickness is not continuous on a microscale. Films above 10 \( \mu \)m were continuous.

![Figure 14 - Top down backscatter SEM, and EDX of copper region, for 5 \( \mu \)m thick film.](image)

Table 3 - Adhesion results by copper thickness, showing that a 15 \( \mu \)m thickness showed good adhesion.

<table>
<thead>
<tr>
<th>SAMPLE</th>
<th>COPPER THICKNESS (( \mu )m)</th>
<th>ADHESION</th>
</tr>
</thead>
<tbody>
<tr>
<td>092407</td>
<td>5.0</td>
<td>POOR</td>
</tr>
<tr>
<td>121916</td>
<td>10.0</td>
<td>POOR</td>
</tr>
<tr>
<td>121904</td>
<td>12.6</td>
<td>POOR</td>
</tr>
<tr>
<td>121910</td>
<td>13.4</td>
<td>FAIR</td>
</tr>
<tr>
<td>092401</td>
<td>15.2</td>
<td>EXCELLENT</td>
</tr>
<tr>
<td>121905</td>
<td>16.7</td>
<td>EXCELLENT</td>
</tr>
<tr>
<td>092403</td>
<td>17.3</td>
<td>EXCELLENT</td>
</tr>
<tr>
<td>092406</td>
<td>20.7</td>
<td>GOOD</td>
</tr>
</tbody>
</table>
Current efficiency

One measure of quality of plating is the current efficiency. Originally developed by Michael Faraday, current efficiency was used to confirm that plating results are theoretically justified. Current, weight gain and time are related by equation 2:

\[
\text{Current efficiency} = \frac{100 \times \text{Deposit weight obtained (g)}}{I \times t \times m / 96485 \times n}
\]  

(2)

If the efficiency is less than 25% or more than 100%, the results are suspect. Current efficiency was highest for copper, followed by nickel, silver, tin and gold (Fig. 15). The efficiency (average of all readings) for copper, silver and nickel was near 1, as expected by theory, but tin and gold were below 1.

![Figure 15 - Efficiency (average value) of films.](image)

Electroless plating

Based on the SEM results in Fig. 14, an attempt was made to increase the density of nucleation sites for copper electroplating by electroless copper plating. This would allow for electroplated layers thinner than 10 μm to adhere well.

Seven of 22 samples were electrolessly plated successfully, a yield of 31.8%. These samples were pink and conductive. Weight gain varied from 0.2 to 2.1 mg/min, which converts to 0.4 to 1.2 μm/min, a thickness range of 2.0 to 23.6 μm. Paradoxically, there were samples with as much weight gain (that did not change color) that did not apparently have copper. The lack of copper was confirmed using EDX. This result did not occur with the electroplating results, which were all affirmative for samples with weight gain. No electroplated samples had weight gain without color change or EDX verification of the plated film. Unlike the electroplating results, the weight gain did not correlate with copper color. Possible causes for film deposition not being repeatable are the surface treatment by 10% sulfuric acid not being aggressive enough (boiling may be needed or other treatment needed - nitric acid14); sensitizing by palladium and tin not being effective or sufficient, possibly due to low temperature; and contamination of the copper plating solution. Further study will be required to elucidate these mechanisms so that thinner layers of copper can be used for solder connectors.

Conclusions

Using commonly available plating chemicals, carbon nanotube tapes and yarns were plated with copper, silver, nickel, tin and gold. Adhesion was excellent. These plated films will aid in the development of aircraft and space cable assemblies by enabling attachment mechanisms for CNTs, which replace copper and save on weight to extend flight range.
Acknowledgements

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References


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Mike Sereda is a PVD Engineer at Materion Large Area Coatings in Windsor, CT, developing and sustaining medical device films on roll-to-roll plastic. He comes from a distinguished career in sputtering, evaporation, plasma spray and fab processing of flexible, wafer and glass substrates, in startups such as Senergen Devices and large companies such as Linear Technology. He recently completed an M.S. in Materials Engineering at San Jose State University to complement his B.S. from MIT.